



TITLE OF INVENTION

**DETERMINATION OF ASCERTAINING AC PATH STATES BY  
FLOATING CONTROLS**

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5 CROSS-REFERENCE TO RELATED APPLICATIONS

Not Applicable

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH

Not Applicable

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REFERENCE TO SEQUENCE LISTINGS

Not Applicable

BACKGROUND OF THE INVENTION

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The present invention relates to electronic controls that must determine ascertain if a path of an ac circuit is intact or open. Typically this means determining ascertaining whether a an ac switching component is open or closed, or a whether a an ac functional component is present.

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Typically the state of a component that switches an ac load is determined read using optoisolators, transformers or other active isolating components to interface ac voltages to electronic control level voltages. There is no electrical connection between ac and the control voltages through the isolating component.

Alternatively a low voltage switch acting in mechanical unison with the ac

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switch is read by the control to indirectly determine ascertain the state of the ac switch. One prior passive component approach with an isolated supply requires a conditioning circuit between ac nodes and works only when the neutral line is the one switched. Other prior passive component approaches only work on supplies that are not isolated from ac. They require a fixed voltage between the control voltages and the ac source.

The approach of using optoisolators or active isolating components requires the use of multiple components for each input to the control. Typically these components include at a minimum an optoisolator, a current limiting resistor on the input and a pull-up resistor on the output. The cost of these 5 components and their assembly add significantly to the cost of electronic controls. The use of active isolating components and the number of components reduce the reliability of this approach.

Using a separate control voltage switch incurs the expense of the switch and the extra connectors and wires to interface it to the control. There is 10 additional expense of mounting hardware and labor. The reliability of mechanical systems is typically far less than a solid state approach.

A technique to interface an electronic control to ac using a resistor, is shown in AN521 of Microchip's Embedded Control Handbook. In this approach the ground of the control is in common with the ac ground establishing ground as 15 a reference. A resistive connection to hot produces ac source frequency pulses. There is no mention of a means of detecting the state of a node whose connections to hot and/or neutral are not already known. This approach relies on the fixed reference of the common ground that is not present with a floating supply. Proper connections to hot and neutral are assumed. If L1 and neutral 20 were inadvertently reversed in installation the technique will not work.

U.S. Pat. No. 5,202,582 shows a method to determine read the state of an ac switch connecting the load to neutral for a floating control using passive components. This approach requires a conditioning circuit with connections to L1, the load side of the switch and a control input. It is designed to determine 25 ascertain solely the state of a ground side switch of an ac circuit. The conditioning circuit shapes the signal. The shape determines the state of the switch. The signal is not compared to a signal from another ac connection.

This method assumes the correct connections to ac are made during installation, something that is not under the control of the manufacturer. Further 30 this approach requires that neutral be switched leaving the transducers connected

to hot unless a an L1 side switch is also opened when the door is opened.

Finally no method is shown to sense the state of a plurality of ac switches in the same circuit or a plurality of circuits.

U.S. Pat. No. 5,184,026 shows a method that can be used for a plurality of switches. However the method deals with controls ~~whose supply voltages are not isolated from the ac source using supplies that do not isolate ac and supply voltages~~. Supplies that are not isolated bring the possibility of shock or worse should the operator come in contact with any control voltage and hence are avoided in consumer applications. As described the monitoring device requires a reference voltage that is a dc drop from the instantaneously higher of the source lines. ~~To produce such a reference requires multiple components and connections between the source and the control. By fixing the source-supply voltage, the design of each sensing means is independent of other sensing means, the state of ac paths, and the polarity of device connections to ac. However this method produces control voltages that are a shock hazard and The the~~ monitoring device must include a reactive component to block the dc voltage between the ac node and the control for this approach to work. The reactive components used to block dc alter the phase of signal received by the control.

Consumer applications, where there is a very real possibility of improper installation resulting in the device not being grounded as intended and/or hot and neutral being reversed, use isolated power supplies, and only the chassis is grounded. This prevents a failure of the isolation from rendering the chassis “live” in an improperly grounded device. Therefore it is desirable to create a low cost sensing means that works with an isolated power supply, regardless of the polarity of the device ac connections and for all ac path states.

#### BRIEF SUMMARY OF INVENTION

The present invention connects ac nodes and digital nodes of a control with a floating power supply to ~~determine~~ ascertain the state of ac path(s) in the circuit containing the ac nodes. The digital nodes of the present invention are

either digital inputs or the supply voltages for the digital circuitry. The electrical connections are made through passive components. The ac potential between the source and the control drives the digital nodes. The subsequent signals on digital nodes are compared to determine interpret the state of ac path(s).

5       The present invention uses high impedance inputs and/or adjusts the impedance between the source and supply to ensure sufficient signal to drive the inputs. The values of input impedance and connection impedance are adjusted to ensure the proper signal for all ac path states that must be discerned. In the  
10       general case this includes testing for all ac power connection possibilities, including a proper or improper ground as all can affect signal strength.

15       The present invention can determine read the state of a plurality of ac paths. The paths may be anywhere in the ac circuit. The state of the path indicates whether it is intact or open. The state of a path can be used to determine ascertain the state of a switching means. It can also determine ascertain if a functional load component is present. The present invention can also determine ascertain if an ac node is floating, indicating that all ac paths to the node are open.

20       The method may be applied to devices where the polarity of the connection to the ac source is unknown. The method may be used to detect zero crossings. The high impedance connections allow inputs to perform other I/O functions when not reading the state of an ac node. The aggregate source-control impedance may be made sufficient to limit the current to a safe level, preferably preferably below the threshold of sensation, should the operator contact any  
25       control node.

30       The simplest connection, one made by a resistor, is the preferred connection. It ensures that if the digital input has a phase it is the same phase as the driving ac signal. While reactive (energy storing) components may be used in the connections to further distinguish signals they are not required, alter the phase of the signal and add to the cost.

The reliability of the present invention is much greater than the prior approaches given the reduction in the number of interface components.

Additionally resistors, the preferred passive component in the connections, are most reliable electrical components.

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## BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is the schematic of the control used to operate the dishwasher in the first embodiment.

10 Figures 2A-E are graphs of voltage versus time occurring on the inputs of the controls in the first and second embodiments.

Figure 3 is the schematic of the control used to operate the dishwasher in the second embodiment.

15 Figure 4 is the schematic of the optional control used to operate the dishwasher in the second embodiment.

## DETAILED DESCRIPTION OF THE INVENTION

Although both the following embodiments are 120vac dishwashers it is to be understood that the inventor contemplates the invention being applied to other devices with the same or different ac transducers and switching means operating off various ac voltages.

### First Embodiment

This embodiment is a dishwasher control. The schematic for the first embodiment is shown in Figure 1. The ac transducers are a motor **70**, a heating element **80** and a solenoid **60** operating a water inlet valve. Operation of the motor **70** and the heating element **80** can be stopped by either the door switch, **S1** or the ac switching **50** operated by the control electronics **40**. Operation of the inlet valve solenoid **60** can be interrupted by the ac switching **50**, the door switch **S1** or the float switch **S2**.

When correctly installed, line L1 of the ac source is connected to S1 and neutral is connected directly to solenoid 60, motor 70 and heating element 80. The input of transformer 20 is also connected to the ac source 10. The power supply regulator 30 is connected to the output of transformer 20. The power supply regulator 30 produces dc voltages, +5v and Gnd, for the control electronics 40 and the input side of the ac switching 50. The output of the power supply 30 is isolated from the ac source by 20. There is no electrical connection through the supply between ac and the control; source-input voltage is dependent on ac-control electrical connections and the intrinsic impedance between source and control. The control electronics 40 selectively activate the ac transducers using the ac switching module 50. While this embodiment uses a linear power supply the approach is the same for any isolated power supply.

During a wash cycle the control activates and times the operation of each transducer. The control must measure only the time a transducer is active, hence it must be able to determine ascertain the state of the door switch S1. When S1 is opened during transducer operation the control suspends its operation until S1 is once again closed. The water fill is timed, S2 does not open during normal operation. S2 remains closed unless a fault causes the dishwasher to overfill. The control does not monitor the state of S2.

In this embodiment of the present invention the control compares the signals received through resistors R1 and R2, each having an impedance of  $5M\Omega$ , to determine ascertain the state of the ac path containing the door switch, S1. R1 is connected between the unswitched ac source side of S1 and digital input 1 of the control electronics 40. R2 is connected between the opposing side of S1 and digital input 2 of 40. Both inputs have high impedance. Input 1 also serves as a designated counter used to time operation by counting the pulses on its input. The control 40 uses the 60hz signal produced on input 1 to accurately time the operation of the dishwasher. This means the only component unique to determining ascertaining the state of S1 is R2.

When **S1** is opened during operation of any transducer, **S1** is the only break in the ac circuit. The 60hz signals on inputs **1** and **2** are  $180^\circ$  out of phase as shown in Figures 2A and 2B. When input **1** is high, input **2** is low. When **2** is high **1** is low. This is true regardless of the polarity of the connection to the ac source **10**. The signals are the portions of the 60hz sinusoidal wave of the ac source **10** truncated by internal protection diodes of inputs **1** and **2**. The signals are limited to +5.6v and -0.6v as long as **R1** and **R2** have sufficient resistance to limit the current through the protection diodes. Further **R1** and **R2** limit the current from the ac source **10** to less than the threshold of sensation providing shock protection in the event the operator contacts a control level node.

When the door switch **S1** is closed, inputs **1** and **2** ~~received~~ receive the same signal (Figure 2A) since **R1** and **R2** are connected to the same ac potential. In this embodiment the intrinsic impedance between the supply voltages and the source **10** complete the input-source loop. The high input impedance of **1** and **2** ensure that the fraction of the ac source voltage dropped across these inputs is sufficient to alter the state of each input. If more input current (a max of  $1\mu\text{A}$  is needed to alter the state of this type of input) were needed and/or if the intrinsic impedance was larger, a connection to opposing ac could be added to ensure signal strength. Thus anytime **1** and **2** are both high or both low **S1** is closed.

In this embodiment there is no need to ~~determine~~ ascertain the state of **S1** when no transducer is selected since the operation of the control is unaffected. Should the operation call for the activation of a transducer when the door has previously been opened, the control will use the ac switching means **50** to select the transducer. After a transducer is selected the control will detect the open door just as it would when the door is opened when a transducer is active. The control will then suspend operation until **S1** is closed.

If it were necessary to ~~determine~~ ascertain the state of **S1** when no transducer is selected by **50** the control must be able to ~~determine~~ ascertain that the ac node of **R2** is floating, isolated from both L1 and neutral. When the switched side of **S1** is isolated, the signal at **2** has approximately a  $90^\circ$  phase

shift to the signal on **1** as shown in Figure 2C. The signal is caused by the intrinsic impedance between the source and the switched side node of **S1**. The signal on **2** will not be low the entire time **1** is high as it is when **S1** is the only break in the circuit. Scanning is done over the period **1** is high. If **2** goes low  
5 anytime during this period **S1** is open.

While the ability to distinguish when the **R2** ac node is floating adds no expense in term of hardware the trade off is in more involved scanning. When the only signals the control needs to detect are those in Figures 2A and 2B detection can be made at any instant other than when the signals are changing  
10 state. The second embodiment demonstrates a means of connecting to ac nodes so that the scan to detect floating nodes is simplified.

## Second Embodiment

In this embodiment resistors **R3-R9** are added to the control as shown in  
15 Figure 3. Components introduced in the first embodiment perform the same function unless noted in the text. The mechanics of the washer are the same as the first embodiment except fill stops when the float switch **S2** opens rather than being timed. This control monitors the states of **S1** and **S2**. The control also monitors the functionality of inlet solenoid **60** and heating element **80** by  
20 connecting resistors **R3** and **R4** between them and inputs **3** and **4** respectively.

In this embodiment resistors **R5-R7** reduce the impedance between inputs **2-4** and control ground. Instead of the signal in Figure 2C, a floating node in this embodiment produces the signal in Figure 2D. The small magnitude of this signal ensures that it is read as a fixed low. Unlike the signals in Figures 2A-C  
25 this signal has no detected phase. In Figure 2, the signal in 2D is easier to distinguish than the signal in 2C from the signals in 2A and 2B. In this embodiment the simplified scanning required to distinguish the 2D signal allows the use of a lower cost CPU (not shown) with less memory thus recovering the cost of including **R5-R7**.

R8 and R9 bias the control relative to the source ensuring that when a sensed ac node is at either line potential the signal in Figures 2A or 2B is produced. Choosing R9< R8<<R1-R4 performs two functions: 1) it biases the control nearer what is nominally neutral allowing a state change on input 1 to 5 serve as a zero crossing detector. 2) when the ac nodes for inputs 1-4 are at the same line potential it prevents the control from becoming so closely biased to that ac line that the signal on inputs 2-4 would be reduced to the signal in Figure 2D. Thus in this embodiment only floating ac nodes produce a fixed low signal.

In this embodiment the state of S1 is again determined ascertained by 10 comparing the signal on input 1 with the signal on input 2. When S1 is closed both inputs have the signal in Figure 2A. When S1 is open, the signal on 1 remains the one in Figure 2A. Figure 2B shows the signal on 2 when S1 is open with a transducer selected. Figure 2D shows the signal on 2 when S1 is open with no transducer selected. R5 lowers the input impedance sufficiently to 15 maintain 2 in the low digital state when its ac node is floating. The signals in Figures 2B and 2D are both low when 1 is high. Hence S1 is open if 2 is low when 1 is high. S1 is closed if 2 is high when 1 is high. When S1 is open the control suspends operation.

In this dishwasher S2 determines the fill level. S2 is closed until the fill 20 level is reached when it opens breaking the circuit of the solenoid 60. During fill the signals on inputs 2 and 3 are compared. They are in phase until S2 opens. This is true regardless of the state of S1. If S1 remains closed when S2 is open the signals on inputs 2 and 3 are those of Figures 2A and 2B. If both S1 and S2 open the signals are those of Figures 2D and 2B. Thus if input 2 is low 25 when input 3 is high S2 is open. When S2 opens the control proceeds to the next step in the wash cycle after the fill.

To determine ascertain the functionality of the solenoid of 60 and the heating element 80 the control scans their paths when their transducers are 30 inactive. An intact path indicates a functional transducer. If a path is open, its transducer is non-functional either because it or a part of the circuit has failed.

The signal on input **1**, Figure 2A, is used as a reference. A functional component will produce the signal in Figure 2B regardless of the polarity of the connections to ac **10**. If the transducer is non-functional the ac node tested will be floating producing a fixed low signal (Figure 2D) on its digital input. Inputs **3** and **4** are 5 scanned when **1** goes low. If **3** is high the solenoid of **60** is functional. If **4** is high the heating element **80** is functional. If **3** is low **60** is non-functional. If **4** is low **80** is non-functional.

All connections of the present invention, not just **R8** and **R9** together with the intrinsic impedance between all nodes and the source, bias the control 10 relative to the source. When an ac path state produces the signal in Figure 2D and/or Fig 2E a supply node can be used as a reference signal. In the circuit in Figure 3 ground can be used as a reference signal to determine ascertain the functionality of the heating element **80** and the inlet valve **60** respectively. If either input remains at zero for one ac source period, 16.7 msec, its respective 15 transducer has failed.

Neither method can determine ascertain the functionality of the heating element **80** at any instant, though when the signal on input **1** is used as a reference functionality can be determined ascertained anytime **1** is low. The addition of diode **D1** and capacitor **C1** as shown in Figure 4 removes the phase of 20 the signal detected by the input **4**. When **80** is functional the signal on input **4** as is shown in Fig 2E in. If **80** is non-functional the signal remains that in Figure 2D. These signals can be distinguished at any instant.

In this embodiment, zero crossings are detected when input **1** changes state. The accuracy of this method depends on where the control ground is 25 biased. The closer the control is biased to the source line not connected to **R1** the greater the accuracy of the zero crossing. Without **R8** and **R9** the bias of the ground is dramatically changed by the state of **S1**, **S2** and the ac switches **50**. This is particularly true when all the transducers are active causing all tested ac nodes to be at the same potential as the unswitched side of **S1**. Selecting **R9**<**R8**

<< **R1-R4** minimizes the affect the state of the ac nodes sensed by **R1-R4** has on the bias of control ground.

In both of the embodiments the aggregate source-control impedance is sufficient to limit the current to below the threshold of sensation should the operator

5 contact any digital node. To guard against a failure of the connecting components resulting in control failure or operator shock multiple components may be used instead of single units. While the state of the switches in both  
embodiments was not set by the control the inventor comtemplates use of the  
invention to verify the correct operation of ac switches (triacs, transistors, relays  
10 or the like) set by the control.